

Singiresu S. Rao, *Reliability Engineering*, Pearson, Upper Saddle River, NJ, 2015

## Chapter 1

### Introduction

#### Answers to Review Questions

##### 1.1

1. Reliability is the probability of a device performing its function over a specified period of time and under specified operating conditions.
2. A component is an integral item which is nonmaintained. A system denotes an assembly of several components which may be maintained or nonmaintained.
3. The graph of failure rate versus time of any mechanical or electronic or other component is known as the bath-tub curve.
4. Failures in early stages of life of a product occur due to manufacturing defects and poor quality control procedures used. As these defective products are replaced or repaired (during the warranty period), the failure rate decreases as time progresses.
5. Because failures occur due to random causes.
6. In mechanical components: due to fatigue brought by a deterioration due to cyclic loading.
7. Air compressor:  $6 \times 10^{-6}$  per hour; Ball bearings:  $1.1 \times 10^{-6}$  per hour; Brakes:  $4.3 \times 10^{-6}$  per hour.
8. AC generator:  $0.8 \times 10^{-6}$  per hour; DC generator:  $36.8 \times 10^{-6}$  per hour; Neon lamp:  $0.49 \times 10^{-6}$  per hour
9. Static, fatigue, creep, corrosion, wear and instability (buckling) modes.
10. Factor of safety = (mean strength/mean load). It is considered inadequate because the same factor of safety implies different values of reliability in different situations.
11. Advisory Group on Reliability of Electronic Equipment. The report recommends that reliability testing must be made an integral part in the development of new systems.
12. Air travel: 9 per year per million persons; Road travel (motor vehicles): 300 per year per million persons.

13. IEEE Transactions on Reliability, Reliability Engineering and System safety.
14. Failure of S. S. Schenectady T-2 tanker: Due to brittle fracture.

## 1.2

1. F
2. T
3. F
4. T
5. F

## 1.3

1. Infant
2. Random
3. Increases
4. Strength, Load

## 1.4

- 1 – c
- 2 – e
- 3 – b
- 4 – a
- 5 – f
- 6 – d

Solutions Manual

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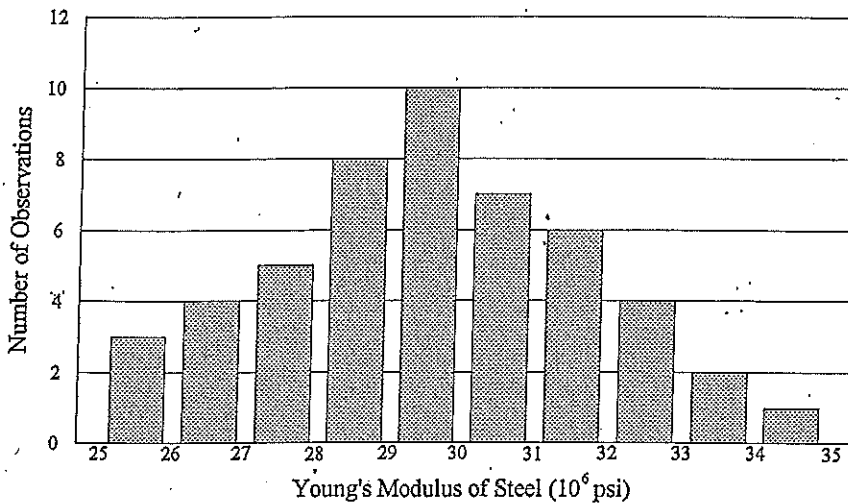
# Chapter 1

## Introduction

1.1  
(a)

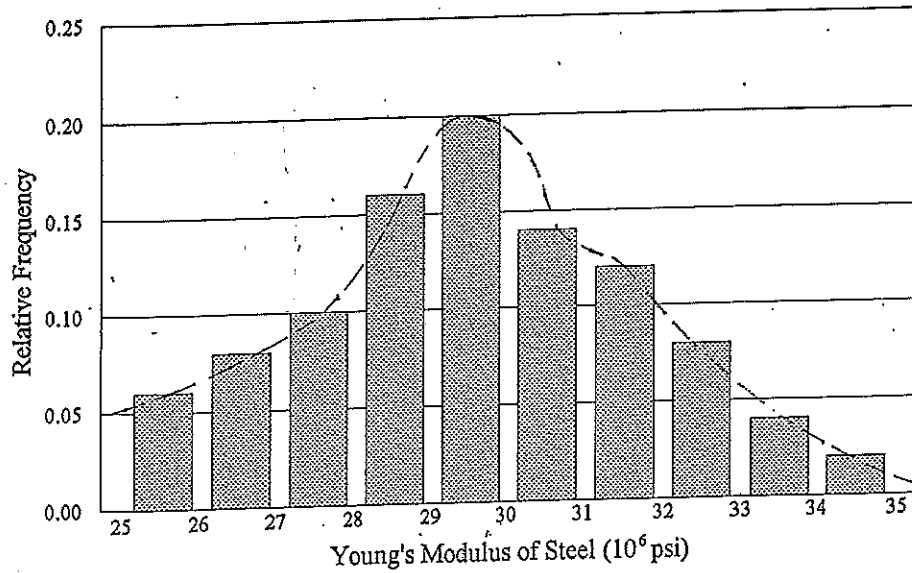
| Data |      |      |      |      | Interval | Observations | Freq  |
|------|------|------|------|------|----------|--------------|-------|
| 25.1 | 27.7 | 29.1 | 30.1 | 31.6 | 25-26    | 3            | 0.060 |
| 25.4 | 27.8 | 29.2 | 30.3 | 31.8 | 26-27    | 4            | 0.080 |
| 25.9 | 28.1 | 29.3 | 30.4 | 31.9 | 27-28    | 5            | 0.100 |
| 26.5 | 28.3 | 29.4 | 30.5 | 32.3 | 28-29    | 8            | 0.160 |
| 26.6 | 28.3 | 29.5 | 30.6 | 32.5 | 29-30    | 10           | 0.200 |
| 26.8 | 28.4 | 29.6 | 30.8 | 32.7 | 30-31    | 7            | 0.140 |
| 26.9 | 28.5 | 29.6 | 30.9 | 32.8 | 31-32    | 6            | 0.120 |
| 27.2 | 28.6 | 29.7 | 31.2 | 33.4 | 32-33    | 4            | 0.080 |
| 27.4 | 28.7 | 29.8 | 31.3 | 33.8 | 33-34    | 2            | 0.040 |
| 27.6 | 28.9 | 29.9 | 31.4 | 34.7 | 34-35    | 1            | 0.020 |
|      |      |      |      |      |          | 50           | 1.000 |

Histogram



(b)

Relative frequency diagram



(c)

| DATA | YOUNG'S MOD | XI - Xave | (XI - Xave)^2 |
|------|-------------|-----------|---------------|
| 25.1 | 25100000    | -4476000  | 2.0035E+13    |
| 29.9 | 29900000    | 324000    | 1.0498E+11    |
| 28.1 | 28100000    | -1476000  | 2.1786E+12    |
| 32.5 | 32500000    | 2924000   | 8.5498E+12    |
| 28.5 | 28500000    | -1076000  | 1.1578E+12    |
| 29.4 | 29400000    | -176000   | 3.0976E+10    |
| 25.4 | 25400000    | -4176000  | 1.7439E+13    |
| 33.4 | 33400000    | 3824000   | 1.4623E+13    |
| 31.9 | 31900000    | 2324000   | 5.401E+12     |
| 26.6 | 26600000    | -2976000  | 8.8566E+12    |
| 26.5 | 26500000    | -3076000  | 9.4618E+12    |
| 31.2 | 31200000    | 1624000   | 2.6374E+12    |
| 29.2 | 29200000    | -376000   | 1.4138E+11    |
| 26.9 | 26900000    | -2676000  | 7.161E+12     |
| 29.3 | 29300000    | -276000   | 7.6176E+10    |
| 30.5 | 30500000    | 924000    | 8.5378E+11    |
| 28.6 | 28600000    | -976000   | 9.5258E+11    |
| 28.3 | 28300000    | -1276000  | 1.6282E+12    |
| 33.8 | 33800000    | 4224000   | 1.7842E+13    |
| 26.8 | 26800000    | -2776000  | 7.7062E+12    |
| 27.4 | 27400000    | -2176000  | 4.735E+12     |
| 32.3 | 32300000    | 2724000   | 7.4202E+12    |
| 29.8 | 29800000    | 224000    | 5.0176E+10    |
| 30.3 | 30300000    | 724000    | 5.2418E+11    |
| 30.4 | 30400000    | 824000    | 6.7898E+11    |
| 31.6 | 31600000    | 2024000   | 4.0966E+12    |
| 29.5 | 29500000    | -76000    | 5776000000    |
| 28.7 | 28700000    | -876000   | 7.6738E+11    |
| 30.9 | 30900000    | 1324000   | 1.753E+12     |

|            |            |                    |            |
|------------|------------|--------------------|------------|
| 27.8       | 27800000   | -1776000           | 3.1542E+12 |
| 28.4       | 28400000   | -1176000           | 1.383E+12  |
| 34.7       | 34700000   | 5124000            | 2.6255E+13 |
| 30.1       | 30100000   | 524000             | 2.7458E+11 |
| 25.9       | 25900000   | -3676000           | 1.3513E+13 |
| 31.4       | 31400000   | 1824000            | 3.327E+12  |
| 32.8       | 32800000   | 3224000            | 1.0394E+13 |
| 30.6       | 30600000   | 1024000            | 1.0486E+12 |
| 29.6       | 29600000   | 24000              | 576000000  |
| 29.6       | 29600000   | 24000              | 576000000  |
| 28.9       | 28900000   | -676000            | 4.5698E+11 |
| 29.1       | 29100000   | -476000            | 2.2658E+11 |
| 27.2       | 27200000   | -2376000           | 5.6454E+12 |
| 31.3       | 31300000   | 1724000            | 2.9722E+12 |
| 27.6       | 27600000   | -1976000           | 3.9046E+12 |
| 32.7       | 32700000   | 3124000            | 9.7594E+12 |
| 28.3       | 28300000   | -1276000           | 1.6282E+12 |
| 31.8       | 31800000   | 2224000            | 4.9462E+12 |
| 30.8       | 30800000   | 1224000            | 1.4982E+12 |
| 27.7       | 27700000   | -1876000           | 3.5194E+12 |
| 29.7       | 29700000   | 124000             | 1.5376E+10 |
|            |            |                    |            |
| TOTAL SUM  | 1478800000 |                    | 2.4079E+14 |
| MEAN VALUE | 29576000   | Lb/in <sup>2</sup> |            |
| STD DEV    | 2194498.58 | Lb/in <sup>2</sup> |            |
|            |            |                    |            |

$$\therefore \bar{X} = 29.5760 \text{ Mpsi} = \text{mean value}$$

$$s_x = 2.1945 \text{ Mpsi} = \text{standard deviation}$$

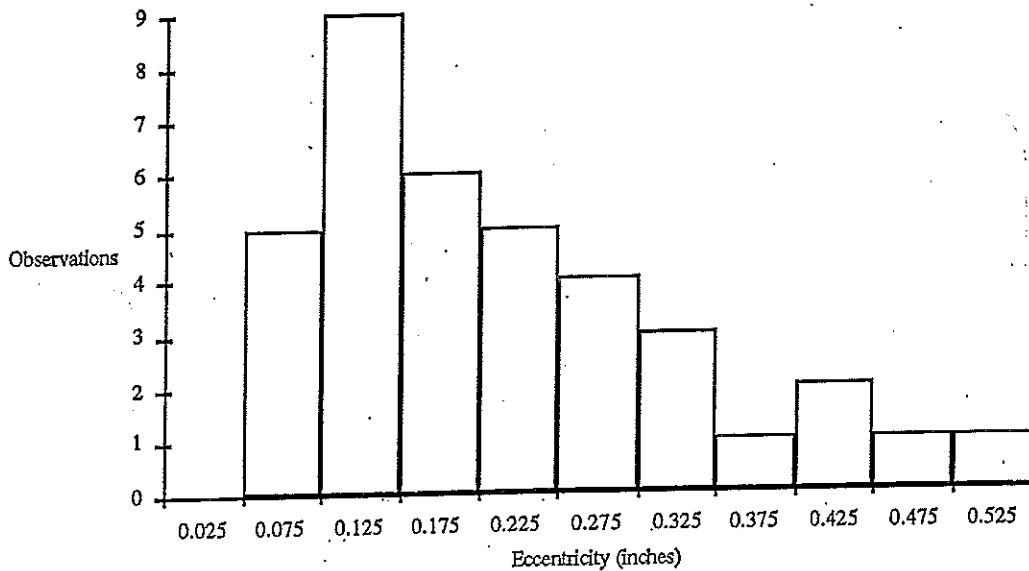
1.2

Observations of eccentricity of applied load

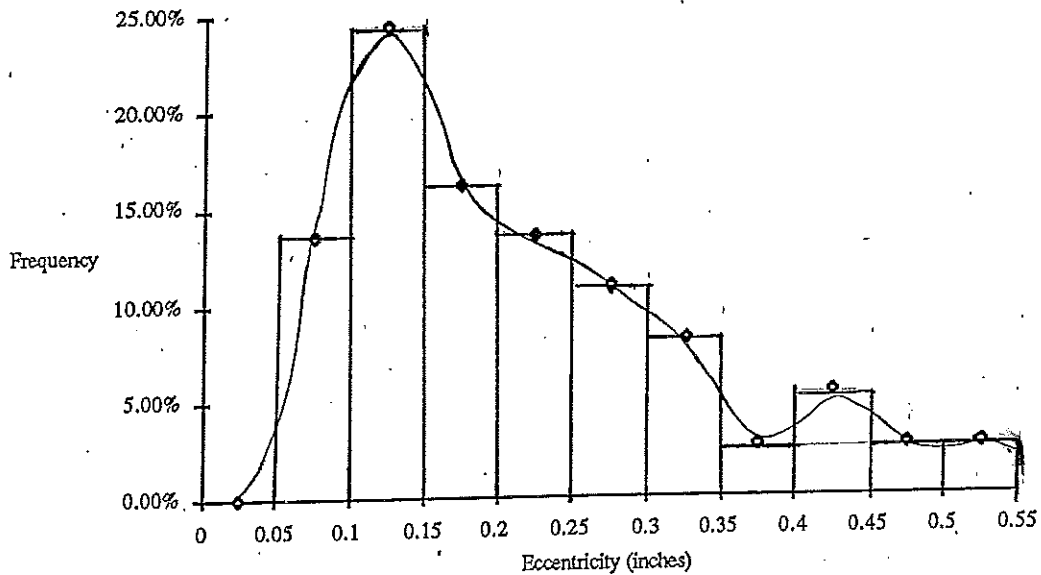
| n  | e<br>inches | $\Sigma e$<br>inches | $\Sigma e^2$<br>inches <sup>2</sup> |
|----|-------------|----------------------|-------------------------------------|
| 1  | 0.410       | 0.410                | 0.1681                              |
| 2  | 0.050       | 0.460                | 0.1706                              |
| 3  | 0.090       | 0.550                | 0.1787                              |
| 4  | 0.195       | 0.745                | 0.216725                            |
| 5  | 0.345       | 1.090                | 0.33575                             |
| 6  | 0.155       | 1.245                | 0.359775                            |
| 7  | 0.320       | 1.565                | 0.462175                            |
| 8  | 0.120       | 1.685                | 0.476575                            |
| 9  | 0.290       | 1.975                | 0.560675                            |
| 10 | 0.065       | 2.040                | 0.5649                              |
| 11 | 0.275       | 2.315                | 0.640525                            |
| 12 | 0.230       | 2.545                | 0.693425                            |
| 13 | 0.140       | 2.685                | 0.713025                            |
| 14 | 0.265       | 2.950                | 0.78325                             |
| 15 | 0.215       | 3.165                | 0.829475                            |
| 16 | 0.070       | 3.235                | 0.834375                            |
| 17 | 0.115       | 3.350                | 0.8476                              |
| 18 | 0.305       | 3.655                | 0.940625                            |
| 19 | 0.435       | 4.090                | 1.12985                             |
| 20 | 0.130       | 4.220                | 1.14675                             |
| 21 | 0.535       | 4.755                | 1.432975                            |
| 22 | 0.110       | 4.865                | 1.445075                            |
| 23 | 0.205       | 5.070                | 1.4871                              |
| 24 | 0.085       | 5.155                | 1.494325                            |
| 25 | 0.135       | 5.290                | 1.51255                             |
| 26 | 0.125       | 5.415                | 1.528175                            |
| 27 | 0.185       | 5.600                | 1.5624                              |
| 28 | 0.480       | 6.080                | 1.7928                              |
| 29 | 0.175       | 6.255                | 1.823425                            |
| 30 | 0.145       | 6.400                | 1.84445                             |
| 31 | 0.380       | 6.780                | 1.98885                             |
| 32 | 0.165       | 6.945                | 2.016075                            |
| 33 | 0.255       | 7.200                | 2.0811                              |
| 34 | 0.180       | 7.380                | 2.1135                              |
| 35 | 0.240       | 7.620                | 2.1711                              |
| 36 | 0.220       | 7.840                | 2.2195                              |
| 37 | 0.105       | 7.945                | 2.230525                            |

| Number of observations in each interval |       |        |        |        |        |        |       |       |       |       |       |
|---|-------|--------|--------|--------|--------|--------|-------|-------|-------|-------|-------|
| From:                                   | 0     | 0.05   | 0.1    | 0.15   | 0.2    | 0.25   | 0.3   | 0.35  | 0.4   | 0.45  | 0.5   |
| To:                                     | 0.05  | 0.1    | 0.15   | 0.2    | 0.25   | 0.3    | 0.35  | 0.4   | 0.45  | 0.5   | 0.55  |
| Midpoint                                | 0.025 | 0.075  | 0.125  | 0.175  | 0.225  | 0.275  | 0.325 | 0.375 | 0.425 | 0.475 | 0.525 |
| Total:                                  | 0     | 5      | 9      | 6      | 5      | 4      | 3     | 1     | 2     | 1     | 1     |
| Frequency:                              | 0.00% | 13.51% | 24.32% | 16.22% | 13.51% | 10.81% | 8.11% | 2.70% | 5.41% | 2.70% | 2.70% |

Column Load Eccentricity Histogram



Column Load Eccentricity Relative Frequency



$$\text{Mean value of eccentricity} = \bar{E} \approx \frac{\mu}{E} = \frac{1}{N} \sum_{i=1}^N E_i = \frac{7.945}{37}$$

$$= 0.215 \text{ inch}$$

$$\text{Standard deviation of eccentricity} = \left\{ \frac{1}{N} \sum_{i=1}^N (E_i - \bar{E})^2 \right\}^{\frac{1}{2}}$$

$$= \left\{ \frac{1}{N} \sum_{i=1}^N E_i^2 - \left( \frac{1}{N} \sum_{i=1}^N E_i \right)^2 \right\}^{\frac{1}{2}} = 0.119 \text{ inch}$$

1.3

29 values of maximum load carried by welded beams given.

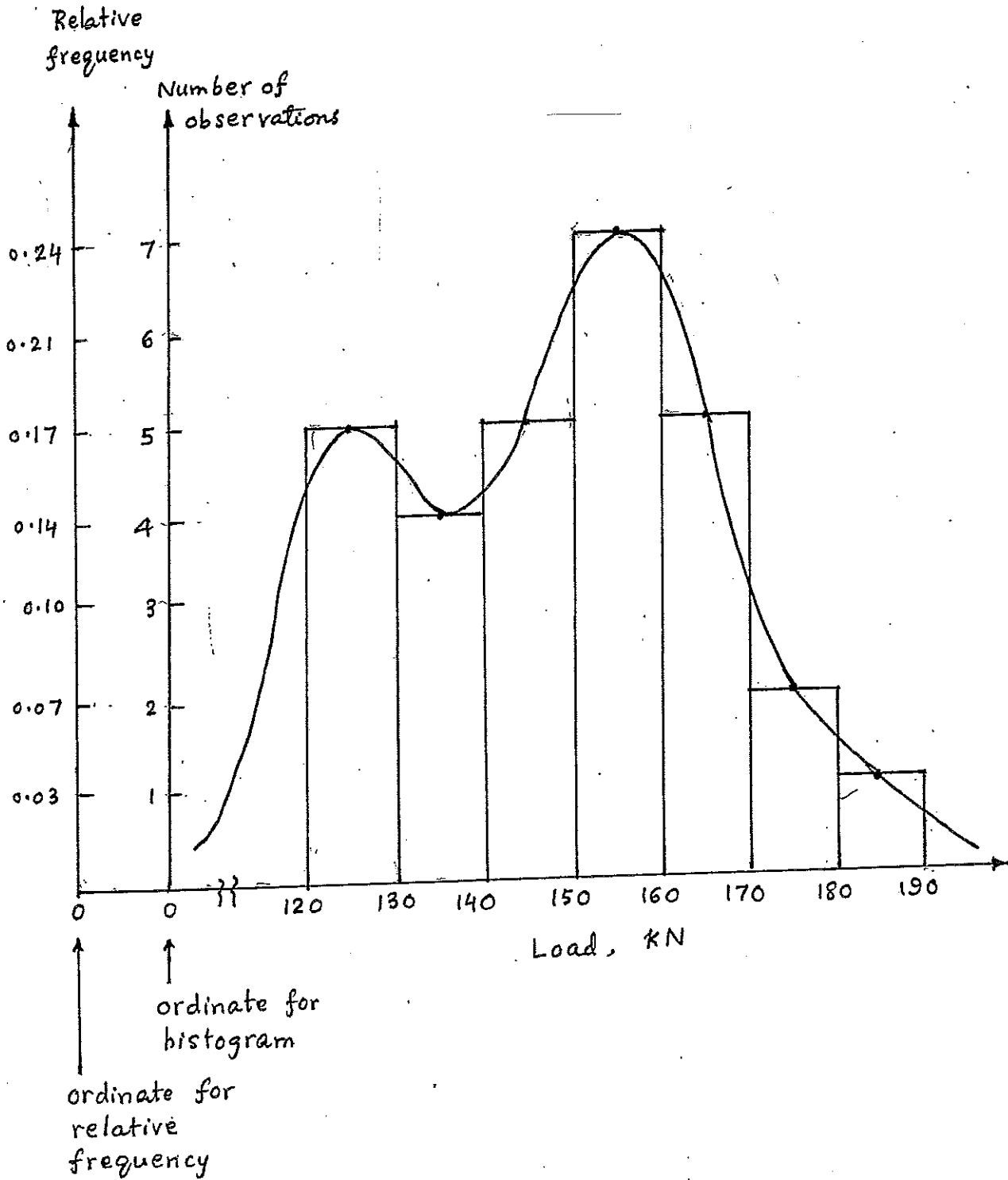
smallest value: 123.1 kN, Largest value: 186.9 kN

Range chosen: 120 kN - 190 kN

All data points are grouped into 7 intervals of 10 kN each.

| Range of load:      | Frequency of load values falling in the range |
|---------------------|---|
| $\geq 120 < 130$ kN | 5   |
| $\geq 130 < 140$ kN | 4   |
| $\geq 140 < 150$ kN | 5   |
| $\geq 150 < 160$ kN | 7   |
| $\geq 160 < 170$ kN | 5   |
| $\geq 170 < 180$ kN | 2   |
| $\geq 180 < 190$ kN | 1   |





1.4 Compressive strength of concrete cylinders, (in kpsi):

Data:

|     |     |     |     |     |              |      |
|-----|-----|-----|-----|-----|--------------|------|
| 5.9 | 6.2 | 5.8 | 7.8 | 6.5 | → $\Sigma =$ | 32.2 |
| 6.3 | 8.9 | 5.3 | 3.7 | 1.4 | → $\Sigma =$ | 25.6 |
| 2.1 | 6.8 | 9.1 | 4.3 | 3.2 | → $\Sigma =$ | 25.5 |
| 7.2 | 6.1 | 5.7 | 4.9 | 2.6 | → $\Sigma =$ | 26.5 |
| 3.4 | 6.8 | 8.3 | 5.1 | 7.3 | → $\Sigma =$ | 30.9 |
| 8.2 | 7.7 | 5.4 | 3.7 | 4.5 | → $\Sigma =$ | 29.5 |
| 4.1 | 5.6 | 6.4 | 6.7 | 7.9 | → $\Sigma =$ | 30.7 |
| 6.9 | 7.5 | 5.2 | 4.3 | 6.6 | → $\Sigma =$ | 30.5 |
| 5.4 | 6.4 |     |     |     | → $\Sigma =$ | 11.8 |

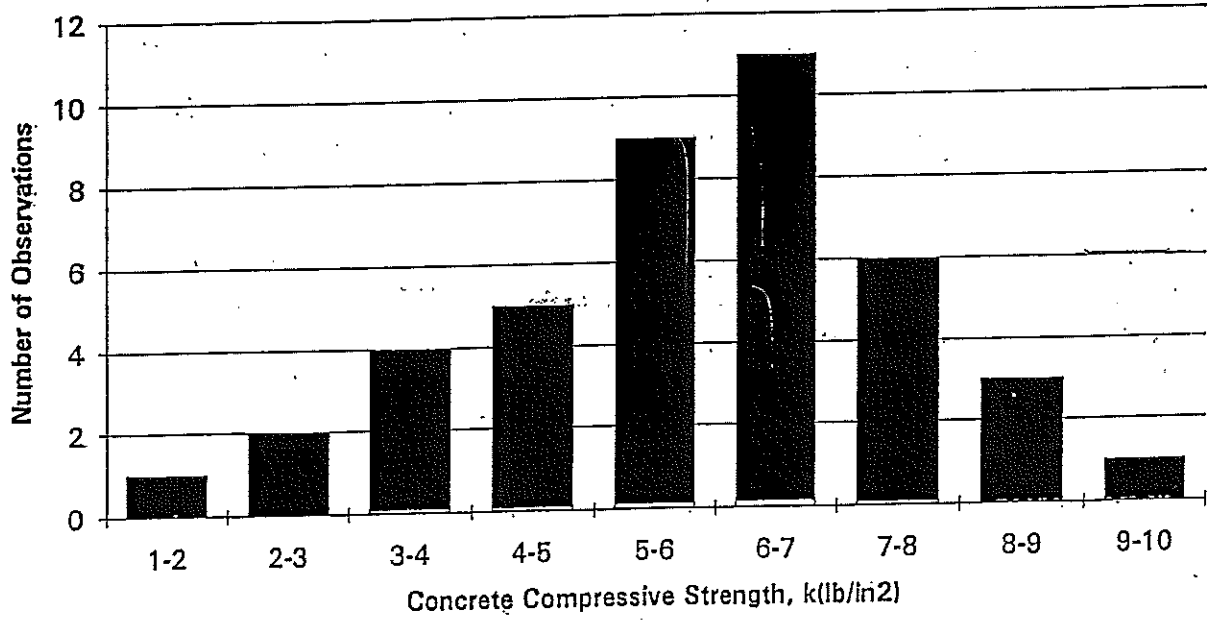
Total sum = 243.2

mean value =  $\bar{x} = \frac{243.2}{42} = 5.79$  kpsi

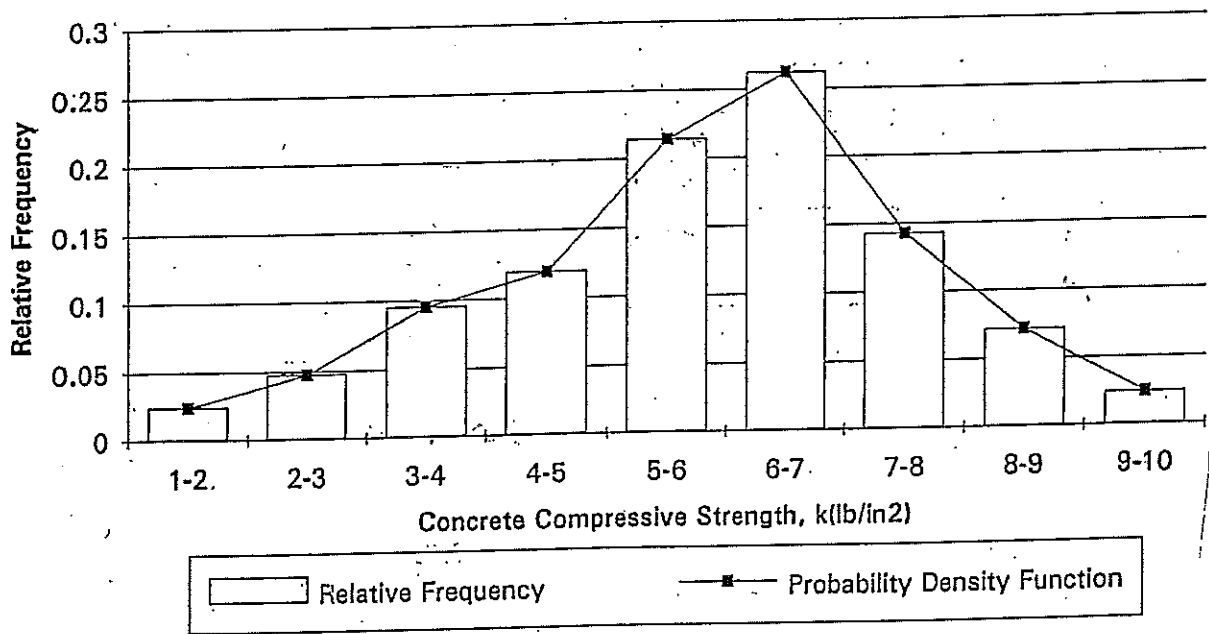
Standard deviation =  $s_x = \left\{ \frac{1}{N-1} \sum_{i=1}^N (x_i - \bar{x})^2 \right\}^{\frac{1}{2}} = 1.81$  kpsi

| Range of compressive strength (kpsi) | Number of occurrences | Relative frequency |
|--------------------------------------|-----------------------|--------------------|
| 1-2                                  | 1                     | $1/42 = 0.024$     |
| 2-3                                  | 2                     | $2/42 = 0.048$     |
| 3-4                                  | 4                     | $4/42 = 0.095$     |
| 4-5                                  | 5                     | $5/42 = 0.119$     |
| 5-6                                  | 9                     | $9/42 = 0.214$     |
| 6-7                                  | 11                    | $11/42 = 0.262$    |
| 7-8                                  | 6                     | $6/42 = 0.143$     |
| 8-9                                  | 3                     | $3/42 = 0.071$     |
| 9-10                                 | 1                     | $1/42 = 0.024$     |

Histogram



Relative frequency diagram



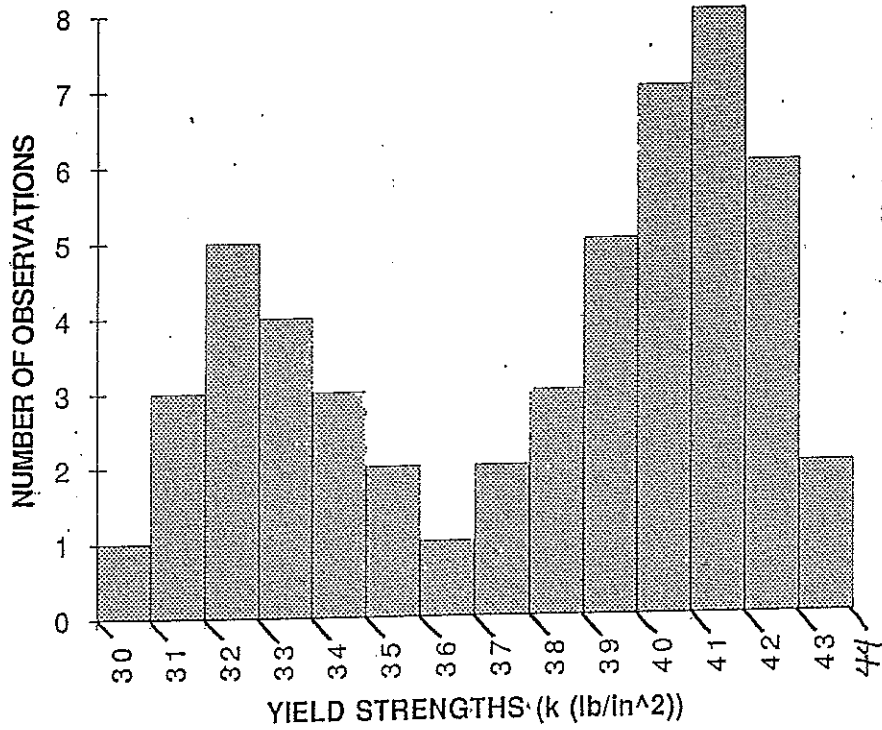
1.5

yield strength data of reinforcing bars (in kpsi)  
made of two different grades of steel:

| Range       | # of Occourances | Relative Frequency |
|-------------|------------------|--------------------|
| 30.0 - 30.9 | 1                | 0.019              |
| 31.0 - 31.9 | 3                | 0.058              |
| 32.0 - 32.9 | 5                | 0.096              |
| 33.0 - 33.9 | 4                | 0.077              |
| 34.0 - 34.9 | 3                | 0.058              |
| 35.0 - 35.9 | 2                | 0.038              |
| 36.0 - 36.9 | 1                | 0.019              |
| 37.0 - 37.9 | 2                | 0.038              |
| 38.0 - 38.9 | 3                | 0.058              |
| 39.0 - 39.9 | 5                | 0.096              |
| 40.0 - 40.9 | 7                | 0.135              |
| 41.0 - 41.9 | 8                | 0.154              |
| 42.0 - 42.9 | 6                | 0.115              |
| 43.0 - 43.9 | 2                | 0.038              |

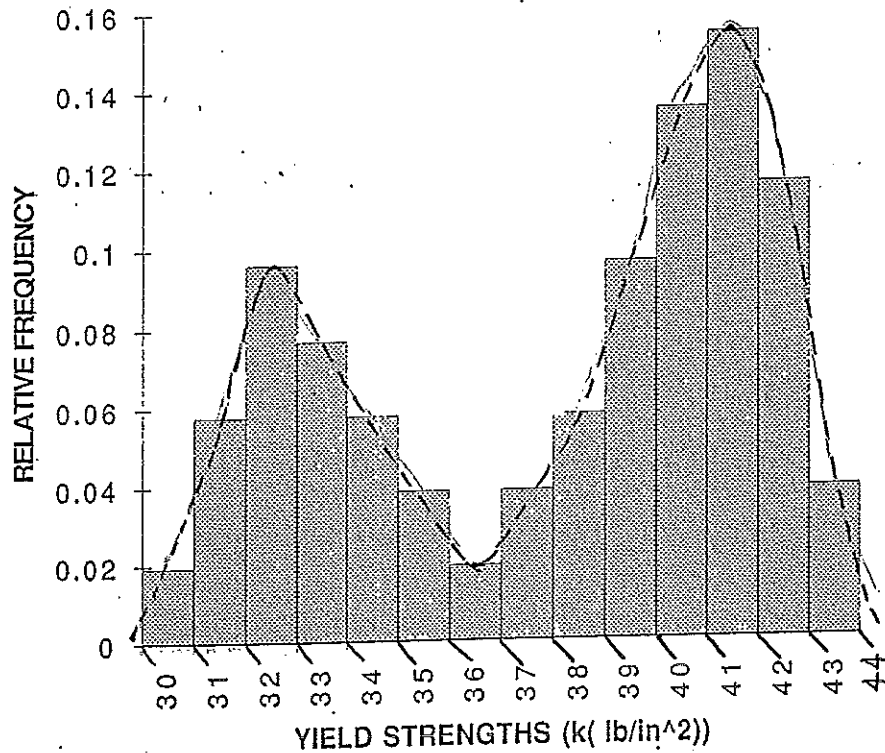
(a)

HISTOGRAM



(b)

RELATIVE FREQUENCY DIAGRAM



(c) The relative frequency diagram has two distinct peaks which shows that the two grades of steel have two different average yield strengths which are approximately 32.5 and 41.5 K(lb/in<sup>2</sup>).

(d)

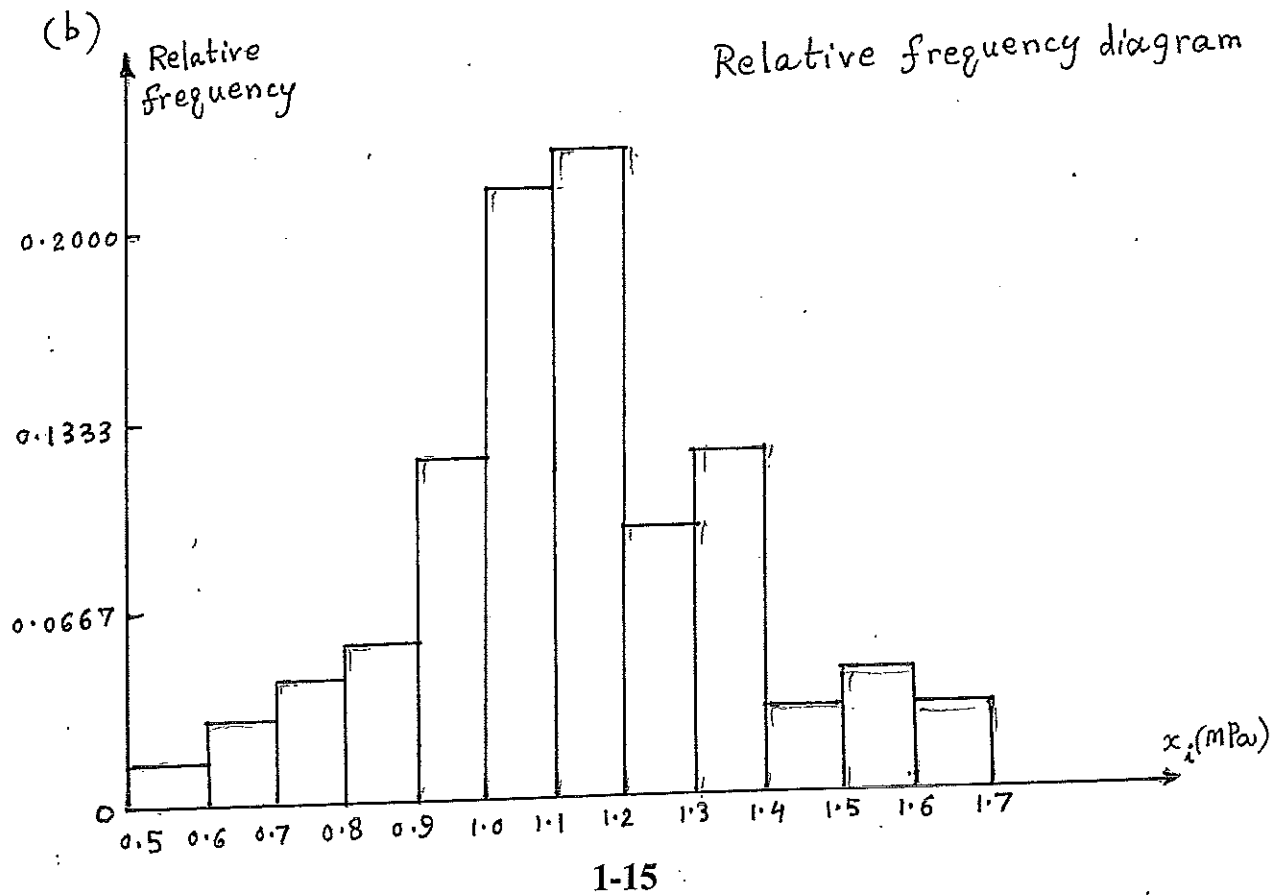
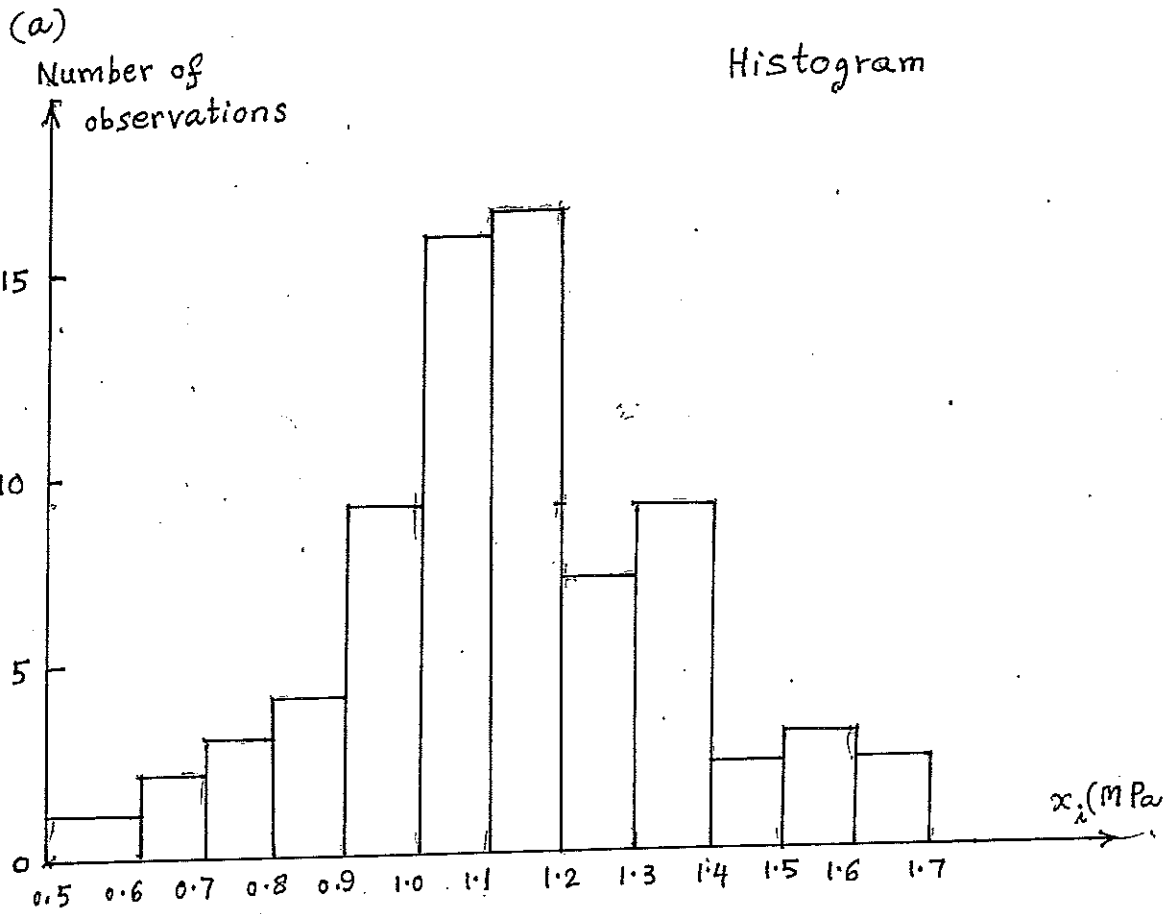
| DATA | Y. STRENGTHS | $X_i - \bar{X}$ | $(X_i - \bar{X})^2$ |
|------|--------------|-----------------|---------------------|
| 35.7 | 35700        | -2315.38462     | 5361005.92          |
| 31.1 | 31100        | -6915.38462     | 47822544.4          |
| 33.2 | 33200        | -4815.38462     | 23187929            |
| 42.5 | 42500        | 4484.61538      | 20111775.1          |
| 41.2 | 41200        | 3184.61538      | 10141775.1          |
| 42.8 | 42800        | 4784.61538      | 22892544.4          |
| 37.5 | 37500        | -515.384615     | 265621.302          |
| 40.7 | 40700        | 2684.61538      | 7207159.76          |
| 42.3 | 42300        | 4284.61538      | 18357929            |
| 42.2 | 42200        | 4184.61538      | 17511005.9          |
| 34.1 | 34100        | -3915.38462     | 15330236.7          |
| 40.9 | 40900        | 2884.61538      | 8321005.92          |
| 43.3 | 43300        | 5284.61538      | 27927159.8          |
| 38.8 | 38800        | 784.615385      | 615621.302          |
| 40.4 | 40400        | 2384.61538      | 5686390.53          |
| 42.9 | 42900        | 4884.61538      | 23859467.5          |
| 38.4 | 38400        | 384.615385      | 147928.994          |
| 41.7 | 41700        | 3684.61538      | 13576390.5          |
| 42.7 | 42700        | 4684.61538      | 21945621.3          |
| 40.1 | 40100        | 2084.61538      | 4345621.3           |
| 41.4 | 41400        | 3384.61538      | 11455621.3          |
| 39.2 | 39200        | 1184.61538      | 1403313.61          |
| 43.4 | 43400        | 5384.61538      | 28994082.8          |
| 40.8 | 40800        | 2784.61538      | 7754082.84          |
| 39.6 | 39600        | 1584.61538      | 2511005.92          |
| 33.8 | 33800        | -4215.38462     | 17769467.5          |
| 36.6 | 36600        | -1415.38462     | 2003313.61          |
| 39.9 | 39900        | 1884.61538      | 3551775.15          |
| 32.3 | 32300        | -5715.38462     | 32665621.3          |
| 32.6 | 32600        | -5415.38462     | 29326390.5          |
| 32.9 | 32900        | -5115.38462     | 26167159.8          |
| 34.5 | 34500        | -3515.38462     | 12357929            |
| 30.2 | 30200        | -7815.38462     | 61080236.7          |
| 38.1 | 38100        | 84.6153846      | 7159.76331          |
| 41.5 | 41500        | 3484.61538      | 12142544.4          |
| 31.2 | 31200        | -6815.38462     | 46449467.5          |
| 31.7 | 31700        | -6315.38462     | 39884082.8          |
| 34.6 | 34600        | -3415.38462     | 11664852.1          |
| 41.1 | 41100        | 3084.61538      | 9514852.07          |

|            |            |             |            |
|------------|------------|-------------|------------|
| 37.2       | 37200      | -815.384615 | 664852.071 |
| 39.5       | 39500      | 1484.61538  | 2204082.84 |
| 39.3       | 39300      | 1284.61538  | 1650236.69 |
| 35.5       | 35500      | -2515.38462 | 6327159.76 |
| 33.7       | 33700      | -4315.38462 | 18622544.4 |
| 32.5       | 32500      | -5515.38462 | 30419467.5 |
| 40.3       | 40300      | 2284.61538  | 5219467.46 |
| 41.8       | 41800      | 3784.61538  | 14323313.6 |
| 32.2       | 32200      | -5815.38462 | 33818698.2 |
| 40.6       | 40600      | 2584.61538  | 6680236.69 |
| 33.4       | 33400      | -4615.38462 | 21301775.1 |
| 41.6       | 41600      | 3584.61538  | 12849467.5 |
| 41.3       | 41300      | 3284.61538  | 10788698.2 |
| TOTAL SUM  | 1976800    | LB/IN^2     | 816187692  |
| MEAN VALUE | 38015.3846 | LB/IN^2     |            |
| STD. DEV.  | 3961.80731 | LB/IN^2     |            |
|            |            |             |            |

1.6 Data on compressive strength of aluminum-lithium specimens (in MPa):

| Interval of compressive strength (MPa) | Number of observed values | Relative frequency value |
|--|---------------------------|--------------------------|
| 0.5001 - 0.6000                        | 1                         | 0.0133                   |
| 0.6001 - 0.7000                        | 2                         | 0.0267                   |
| 0.7001 - 0.8000                        | 3                         | 0.0400                   |
| 0.8001 - 0.9000                        | 4                         | 0.0533                   |
| 0.9001 - 1.0000                        | 9                         | 0.1200                   |
| 1.0001 - 1.1000                        | 16                        | 0.2133                   |
| 1.1001 - 1.2000                        | 17                        | 0.2267                   |
| 1.2001 - 1.3000                        | 7                         | 0.0933                   |
| 1.3001 - 1.4000                        | 9                         | 0.1200                   |
| 1.4001 - 1.5000                        | 2                         | 0.0267                   |
| 1.5001 - 1.6000                        | 3                         | 0.0400                   |
| 1.6001 - 1.7000                        | 2                         | 0.0267                   |
| Total                                  | 75                        | 1.0000                   |





$$(c) \text{ Mean value} = \bar{x} = \frac{1}{75} \sum_{i=1}^{75} x_i = \frac{1}{75} (1.0335 + 0.9302 + \dots + 1.3091)$$
$$= 1.1227 \text{ MPa}$$

$$\text{Standard deviation} = s_x = \left\{ \frac{1}{75} \sum_{i=1}^{75} (x_i - \bar{x})^2 \right\}^{\frac{1}{2}}$$
$$= \left\{ \frac{1}{75} \left[ (1.0335 - 1.1227)^2 + \dots + (1.3091 - 1.1227)^2 \right] \right\}^{\frac{1}{2}}$$
$$= 0.0227 \text{ MPa}$$

(d) From the given data, number of specimens that gave a value of  $x_i$  below 1 MPa = 19 out of 75 =  $\frac{19}{75} = 0.2533$  or 25.33 %.

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